

Eric Marchand, University of Nevada, Reno Andrea Achilli, Humboldt State University Sage Hiibel, University of Nevada, Reno









About WateReuse

The mission of the WateReuse Research Foundation is to build support for water reuse through research and education.

More information

www.watereuse.org/foundation

Research Reports

www.watereuse.org/foundation/publications



Logistical Notes

- Today's webcast will be 60 minutes
- A PDF of today's presentation can be downloaded when you complete the survey at the conclusion of this webcast
- There is one Professional Development Hour available
- If you have questions for the presenters, please send a message by typing it into the chat box located on the panel on the left side of your screen
- If you would like to enlarge your view of the slides, please click the Full Screen button in the upper right corner of the window
- To use the chat box, you must exit full screen



Today's Presenters



Eric Marchand, Ph.D., P.E. University of Nevada, Reno



Andrea Achilli, Ph.D., P.E. Humboldt State University



Sage Hiibel, Ph.D. University of Nevada, Reno







Project Overview

Dr. Eric Marchand



Acknowledgements

- Project Manager Kristan Cwalina
- Project Advisory Committee
 - Chris Haney, Senior Vice President Gresham, Smith and Partners
 - Paul Westerhoff, Professor Arizona State University
 - Charles Bott, Research and Development Manager Hampton Roads Sanitation District (HRSD)
 - Katherine Dahm, Engineer Bureau of Reclamation
- Industry Partners
 - Hydration Technology Innovations (HTI)
 - Porifera
 - Washoe County Department of Water Resources
 - Truckee Meadows Water Reclamation Facility (TMWRF)







Hydration Technology Innovations



Presentation Overview

- Project Objectives
- Coupled Forward Osmosis and Membrane Distillation
- Wastewater Concentration by Forward Osmosis
- Anaerobic Membrane Bioreactor Performance
- Discussion and Questions



Project Objectives

• Conceptualize a novel treatment scheme to reduce energy associated with domestic wastewater treatment

- Conduct a literature review to establish operating conditions for each unit process
- Develop a process model for the treatment scheme and compare performance to an existing water reclamation facility
- Perform laboratory-scale experiments to optimize operating parameters of individual unit processes



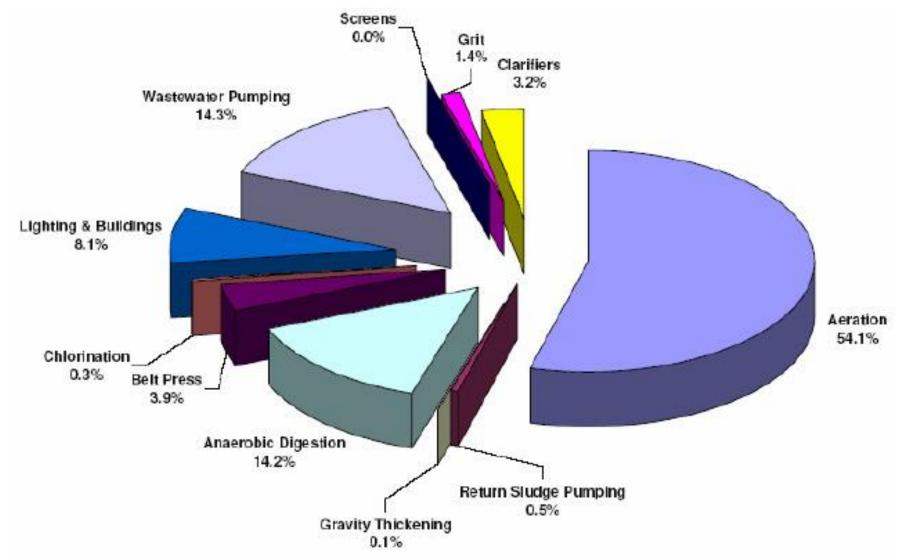
Relevance to WateReuse RFP

- 10-06: Challenge Projects on Low Energy Treatment Schemes for Water Reuse

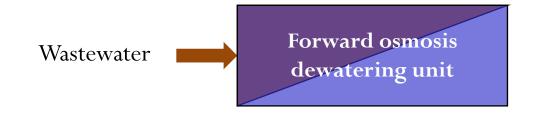
 The goal of the project is to Conceptualize and evaluate alternatives to energy intensive aerated activated sludge systems for providing suitable water for one or more reuse applications, ranging from irrigation to cooling tower water to pretreatment for reverse osmosis or other reuse treatment processes. The project would include two phases, which will be funded separately, a development phase and a testing phase.
- Phase 1 Research Collect literature data and perform preliminary modeling
- Phase 2 Research Test system components in lab setting



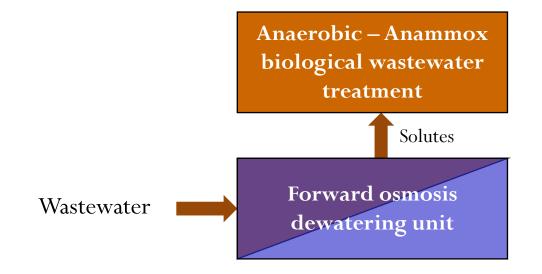
Energy for Wastewater Treatment



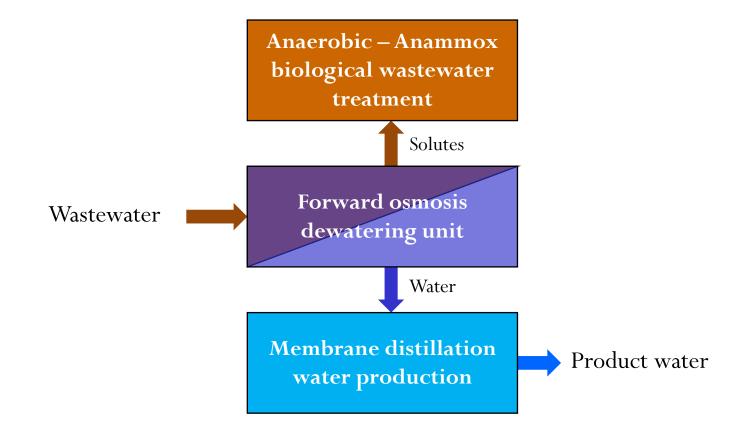




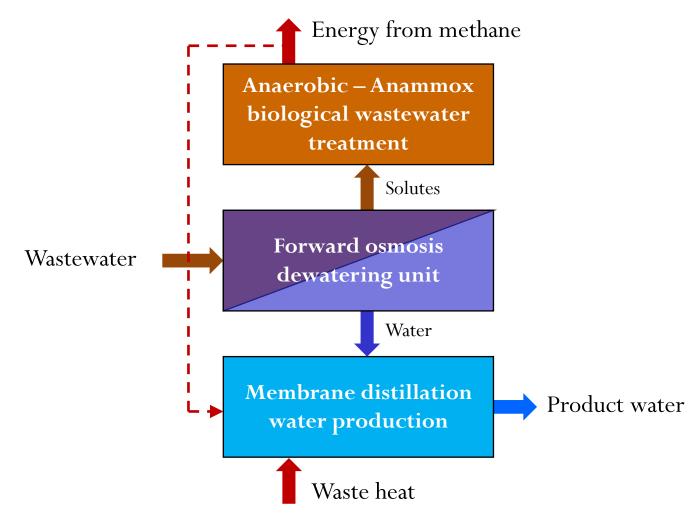




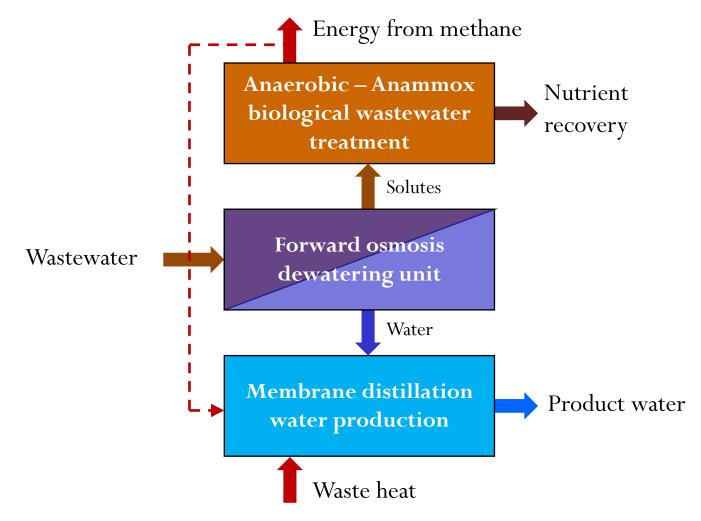




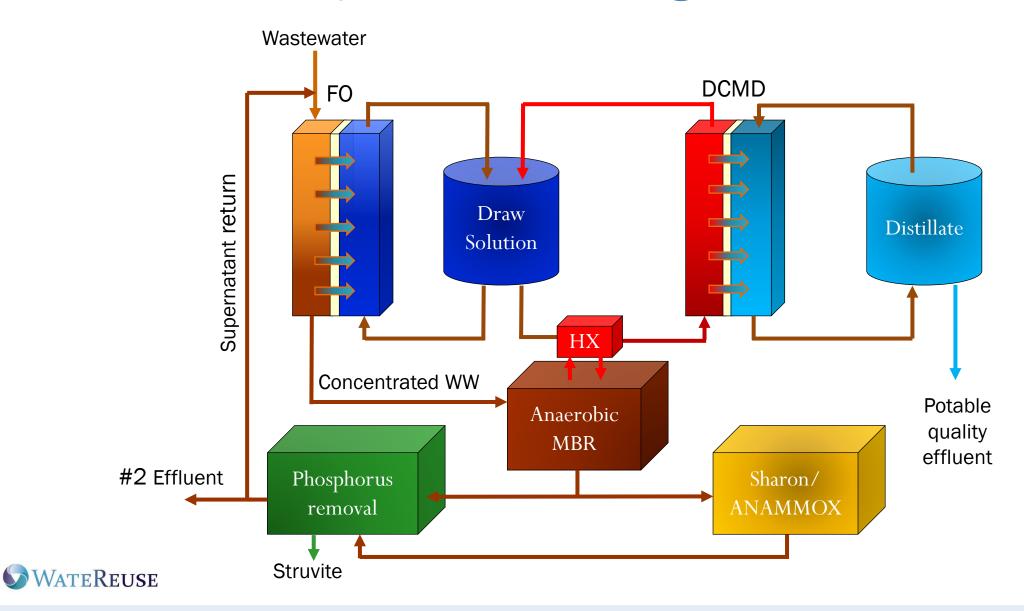


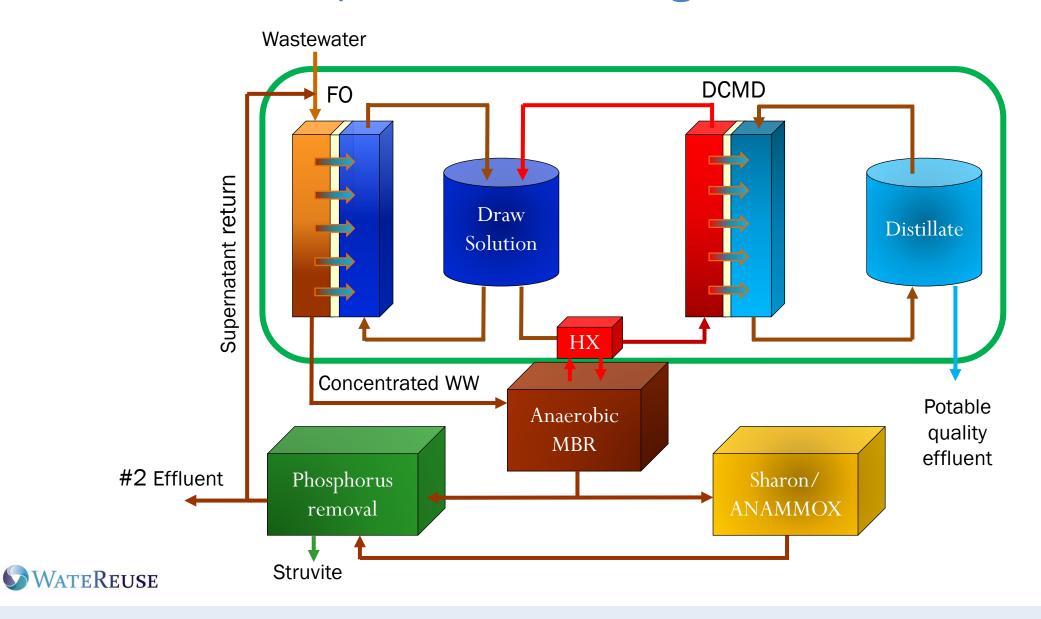


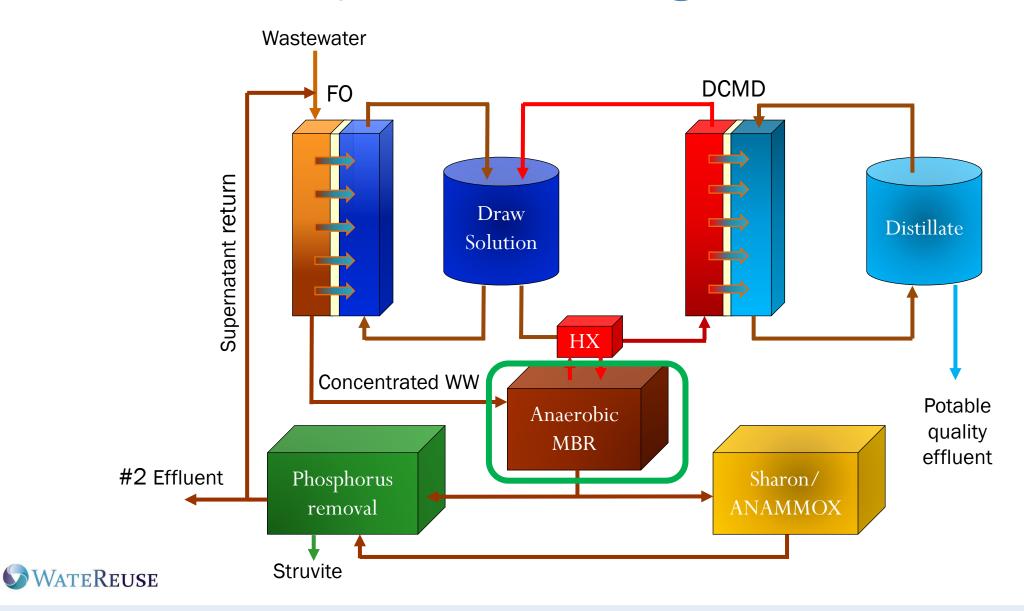


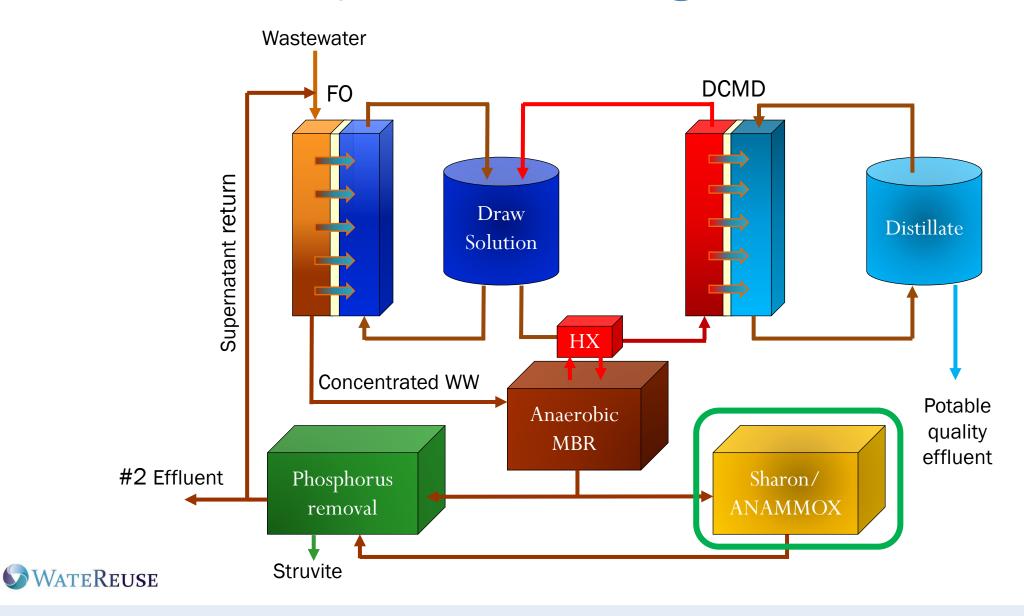


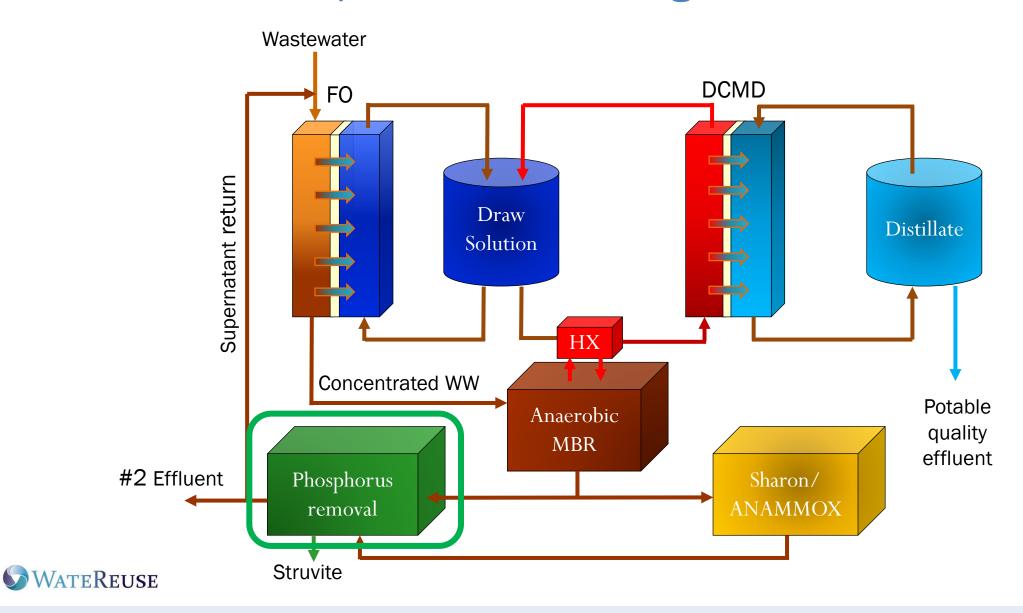












Phase 1: Proof of Concept Testing

- Perform literature review for system components
 - Forward Osmosis
 - Membrane Distillation
 - Anaerobic MBR
 - Sharon Anammox
 - Struvite Precipitation
- Identify typical operating conditions for each process
- Develop BioWin Model
- Perform simulation at two FO recoveries (50% and 70%)
- Compare performance to water reuse facility



Forward Osmosis (FO)

FO serves as a pre-concentration step: clean water in the influent wastewater diffuses across the forward osmosis membrane into the draw solution.

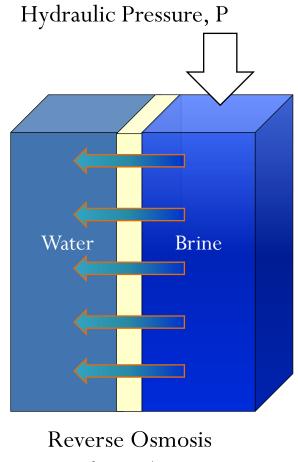


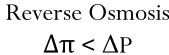
www.htiwater.com

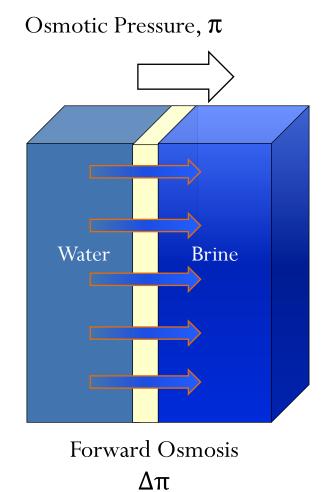
| Parameter | Typical Values | |
|----------------------------------|---------------------------|--|
| Flux (L/m ² *hr, LMH) | 2.7 - 12.9 | |
| Draw Solution | NaCl or MgCl ₂ | |
| Solute Ionic Strength (M) | 2.0 - 5.0 | |
| Water Recovery (%) | 50 - 70 | |
| Reverse Salt Flux | Variable, ∼0.15*Flux | |
| | | |



Reverse Osmosis vs. Forward Osmosis









Membrane Distillation (MD)

MD uses a porous hydrophobic membrane to facilitate the transfer of clean water from a heated feed solution to a cold distillate stream.

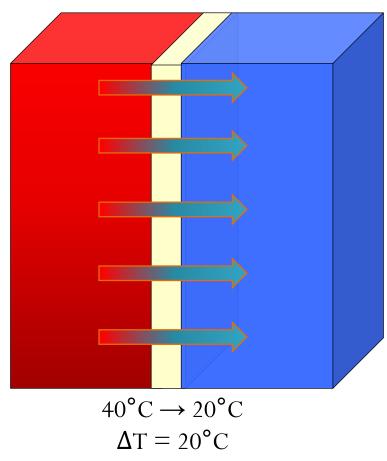


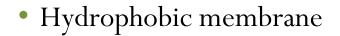
www.advantage-environment.com

| Parameter | Typical Values |
|----------------------------------|----------------|
| FeedTemp (°C) | 40.0 - 80.0 |
| Permeate Temp (°C) | 17.5 - 23.0 |
| Flux (L/m ² *hr, LMH) | 10 - 80 |
| Water Recovery (%) | 80 - 95 |
| Salt Rejection (%) | > 95 |



Membrane Distillation (MD)





- Thermally driven process
- Low energy input



Anaerobic Membrane Bioreactor (AnMBR)

An AnMBR serves two main purposes: removal of chemical oxygen demand (COD) and production of methane biogas.



www.gewater.com

| Parameter | Typical Values |
|----------------------------------|----------------|
| Methane (L/g COD) | 0.2 - 0.35 |
| MLSS (g/L) | 5 – 30 |
| Flux (L/m ² *hr, LMH) | 5 – 8 |
| COD Removal (%) | >80 |
| SRT (days) | > 60 |



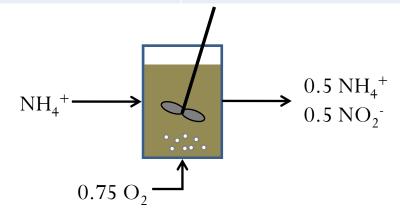
Sharon Process

The SHARON (single-reactor highyield ammonium removal over nitrite) process is known as partial nitrification.

The target result of SHARON is an even molar ratio of ammonium to nitrite.

Incomplete nitrogen oxidation reduces the oxygen required.

| Parameter | Typical Values |
|-------------------------------------|----------------|
| Temp (°C) | 19 – 35 |
| Nitrogen Load (kg/m³*d) | 0.1 - 3.3 |
| NO ₂ -:NH ₄ + | 1:1 |
| HRT & SRT (hr) | 4.8 - 36 |





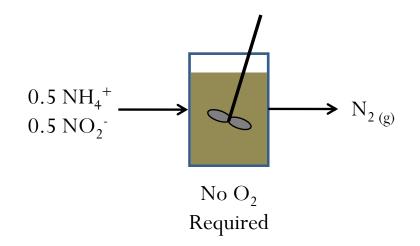
Anammox Process

In the ANAMMOX process (ANaerobic AMMonium OXidation), ammonium is used as an electron donor while nitrite is used as an electron acceptor.

Nitrogen is released from the ANAMMOX process as nitrogen gas.

$$NH_4^+ + NO_2^- \rightarrow N_2 + 2 H_2O$$

| Parameter | Typical Values | | |
|---|----------------|--|--|
| Temp (°C) | 22 - 35 | | |
| SNR (g N/gVSS*d) | 0.15 - 1.15 | | |
| NO ₂ -:NH ₄ +:NO ₃ - | 1:1.2:0.2 | | |





Struvite Precipitation

Struvite (MgNH₄PO₄*6 H₂O) naturally precipitates from wastewater through the addition of magnesium and by increasing pH.



| Parameter | Typical Values |
|------------------|----------------|
| рН | 8 – 9 |
| Temp (°C) | 14.5 - 25 |
| Mg:P Molar Ratio | 1:1 |
| HRT (hr) | < 4 |



www.ostara.com

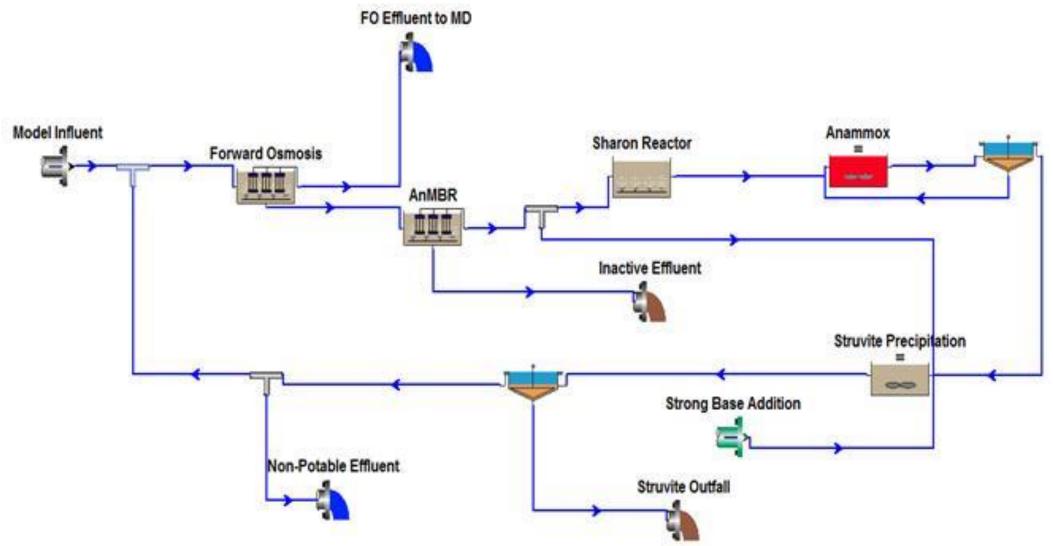
Comparison with Water Reuse Facility in Reno

- Selected 100% water reuse facility for comparison (South Truckee Meadows Water Reclamation Facility, STMWRF)
- Developed BioWin model for conceptual facility
- Evaluated BioWin model with STMWRF inputs
 - Varied FO recovery (50% and 70%)
 - Evaluated model for extreme operating ranges
- Compared costs between facilities





BioWin Model Development





BioWin Modeling Conditions

• Input water quality parameters were based on STMWRF influent

| Parameter | Value | Parameter | Value | |
|------------|------------|------------------|--------------|--|
| Flow | 3 MGD | COD | 300 mg COD/L | |
| TKN | 20 mg N/L | Total Phosphorus | 5 mg P/L | |
| Nitrate | 0.3 mg N/L | рН | 7.3 | |
| Alkalinity | 5.5 mmol/L | Calcium | 45 mg/L | |
| Magnesium | 15 mg/L | Dissolved Oxygen | 0 mg/L | |



Model Results - Cost Breakdown

• Projected cost varied between \$86.3K — \$199.4K per MGD per year

| Process | 50% Recovery (Minimum / Maximum) | | 70% Recovery (Minimum / Maximum) | |
|-----------------------|-------------------------------------|----------|-------------------------------------|----------|
| \$/MGD treated / year | \$107.4K | \$199.4K | \$86.3K | \$188.8K |

- Comparison facility cost: \$96.3K per MGD per year
- Important distinction: Product water from membrane distillation is <u>high quality</u> reuse water



Transition to Phase 2 Research

- Overall feasibility of conceptual model facility was validated
- Cost estimates are reasonable when compared with traditional reuse facility
- Research needed to answer the following questions:
 - 1. How does the <u>coupled</u> FO-DCMD system respond to transient operating conditions?
 - 2. What are the limitations of concentrating domestic wastewater with a FO module?
 - 3. Is AnMBR performance affected by FO pre-concentration?





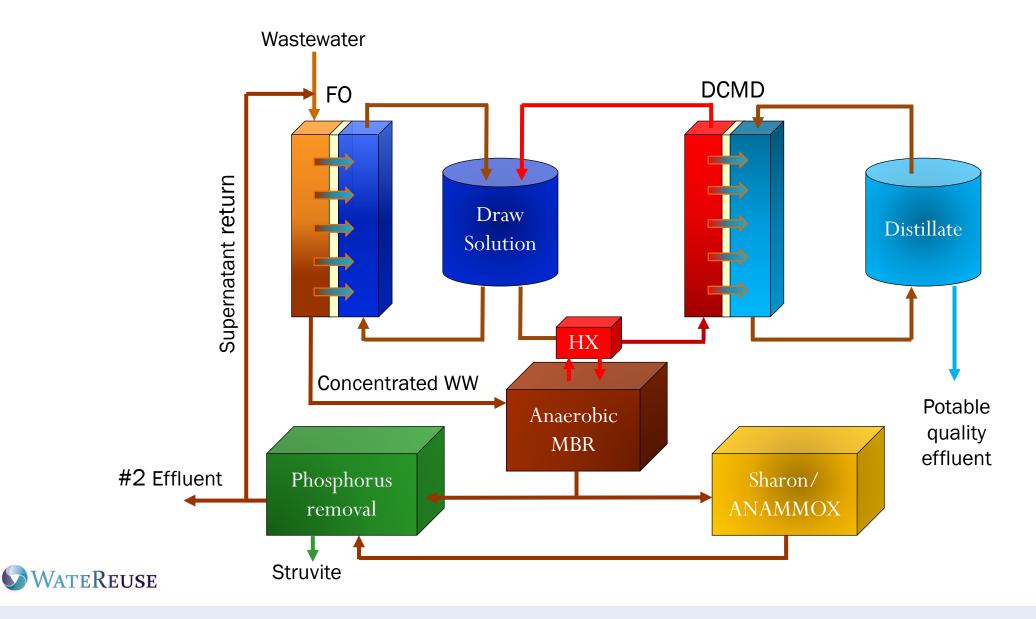


Coupled Forward Osmosis and Membrane Distillation

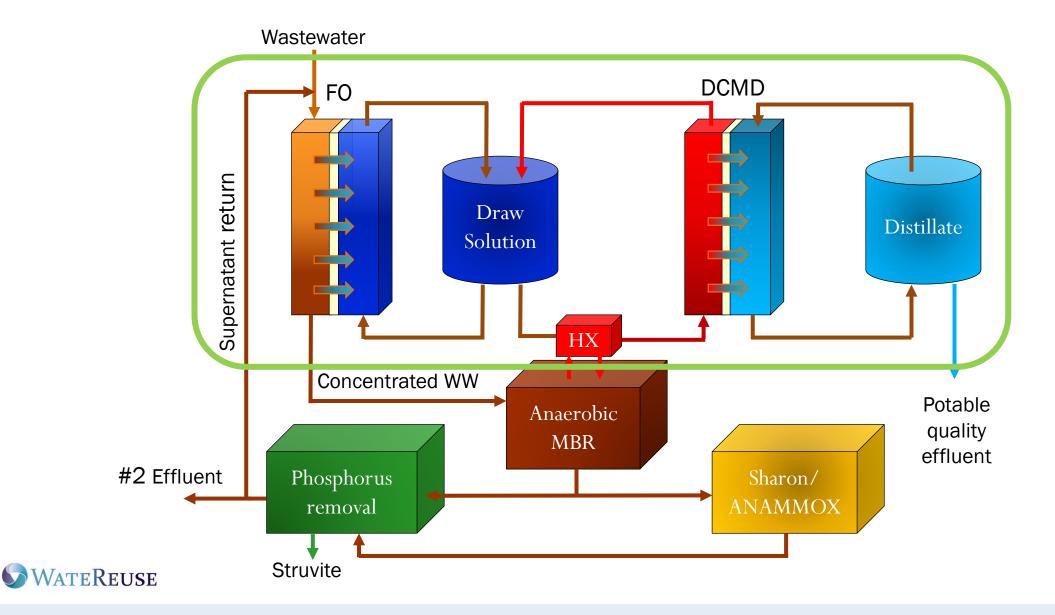
Dr. Andrea Achilli

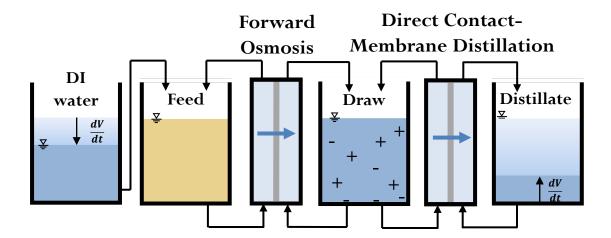


Forward Osmosis and Membrane Distillation

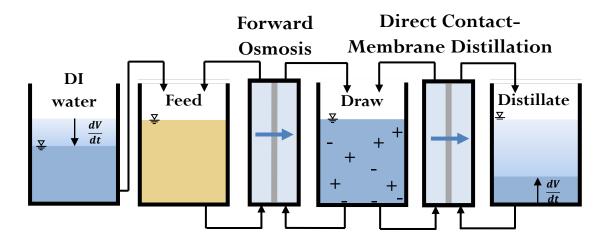


Forward Osmosis and Membrane Distillation



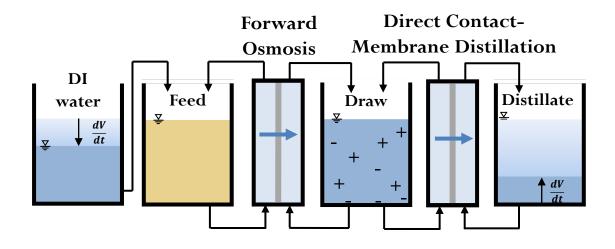






| Experimental Conditions | | |
|-------------------------------------|---|--------------------|
| Draw Solution | = | 35-40 g/L NaCl |
| Pump Flow Rates | = | 1 L/min |
| Forward Osmosis Membrane Area | = | 170 cm^2 |
| Membrane Distillation Membrane Area | = | 140 cm^2 |
| Heated Stream Temperature | = | 35-50 °C |
| Distillate Stream Temperature | = | 20-22 °C |





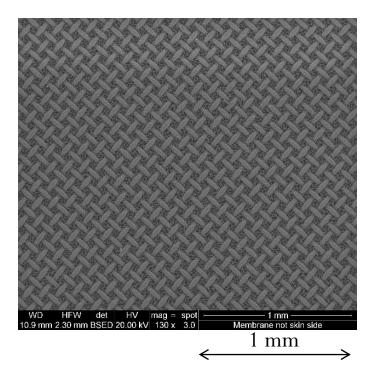
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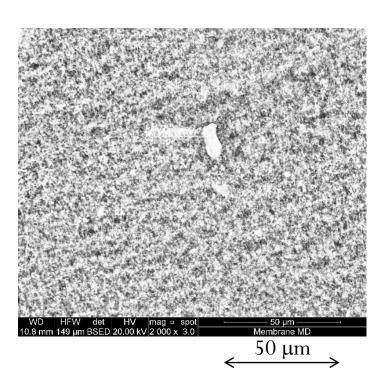


Membranes and Spacers

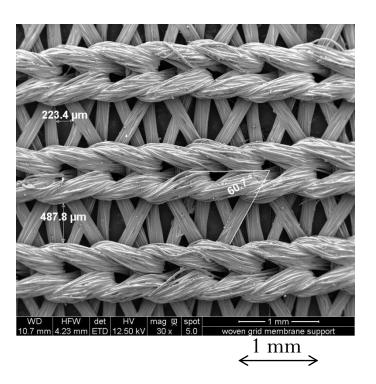
Forward Osmosis Membrane



Membrane Distillation Membrane



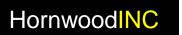
Woven Grid Membrane Support

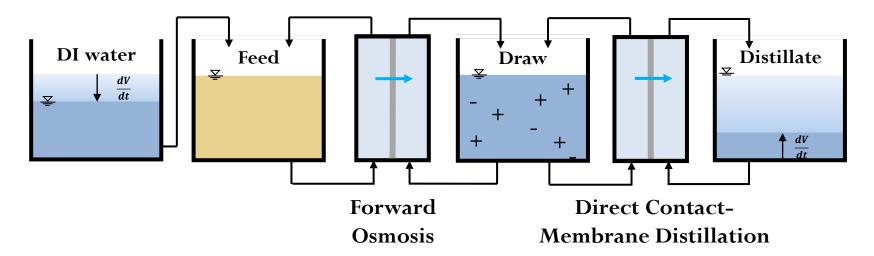




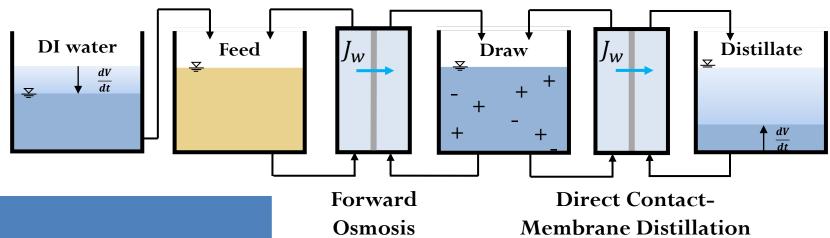








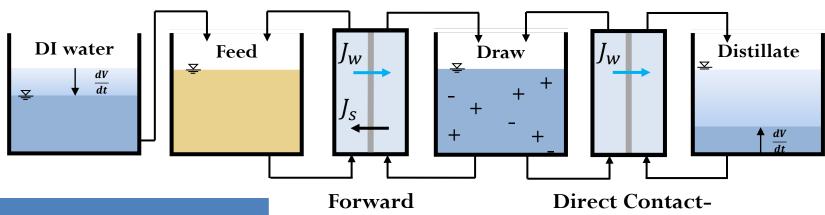




| Where: | | | | |
|-------------|---|---|--|--|
| V | = | Volume [L] | | |
| t | = | Time [hr] | | |
| $A_{\rm m}$ | = | Effective Membrane Area [m²] | | |
| A_{FO} | = | FO Membrane Area [m²] | | |
| C_p, C_f | = | Concentration of Permeate, Feed [mg/L] | | |

| $J_w = Water Flux =$ | $\frac{dV}{dt} \cdot A_m^{-1} [L \cdot m^{-2}]$ | · h ⁻¹] |
|----------------------|--|---------------------|
| | ui | |





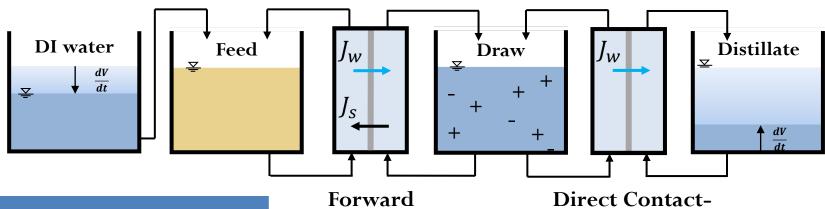
Osmosis

| Where: | | | | |
|-------------|---|---|--|--|
| V | = | Volume [L] | | |
| t | = | Time [hr] | | |
| $A_{\rm m}$ | = | Effective Membrane Area [m²] | | |
| A_{FO} | = | FO Membrane Area [m ²] | | |
| C_p, C_f | = | Concentration of Permeate, Feed [mg/L] | | |

$$\begin{split} J_w &= Water\, Flux = \frac{dV}{dt} \cdot A_m^{-1} \ \left[\mathbf{L} \cdot \mathbf{m}^{-2} \cdot \mathbf{h}^{-1} \right] \\ J_s &= Reverse\, Salt\, Flux = \frac{dc_f}{dt} \cdot V_f \cdot A_{FO}^{-1} \ \left[\mathbf{g} \cdot \mathbf{m}^{-2} \cdot \mathbf{h}^{-1} \right] \end{split}$$

Membrane Distillation





Osmosis

| Where: | | | | |
|-------------|---|---|--|--|
| V | = | Volume [L] | | |
| t | = | Time [hr] | | |
| $A_{\rm m}$ | = | Effective Membrane Area [m²] | | |
| A_{FO} | = | FO Membrane Area [m²] | | |
| C_p, C_f | = | Concentration of Permeate, Feed [mg/L] | | |

$$J_{w} = Water Flux = \frac{dV}{dt} \cdot A_{m}^{-1} \left[\mathbf{L} \cdot \mathbf{m}^{-2} \cdot \mathbf{h}^{-1} \right]$$

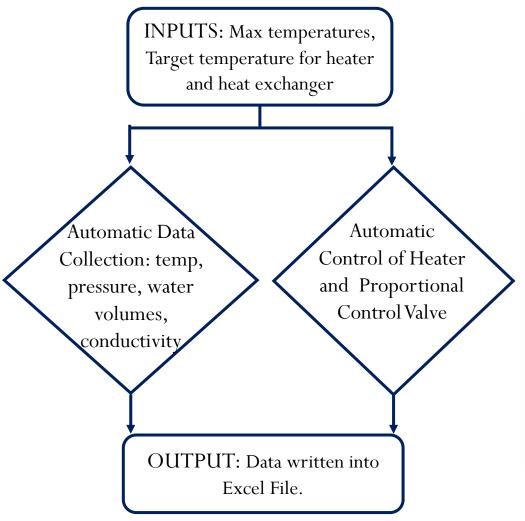
$$J_{s} = Reverse Salt Flux = \frac{dc_{f}}{dt} \cdot V_{f} \cdot A_{F0}^{-1} \left[\mathbf{g} \cdot \mathbf{m}^{-2} \cdot \mathbf{h}^{-1} \right]$$

$$Rejection = \left(\mathbf{1} - \frac{C_{p}}{C_{f}} \right) \cdot \mathbf{100} \%$$

Membrane Distillation



Monitor and Control System



LabVIEW Monitoring and Control





Feed and Draw Solutions

Surrogate Wastewater Feed Solution

| Constituent | C (mg/L) |
|---|----------|
| Nutrient Broth (Peptone:Beef Extract Ratio 5:3) | 180 |
| Humic Acid, Crystalline Powder | 100 |
| Urea | 70 |
| Ammonium Chloride | 70 |
| Monopotassium Phosphate | 50 |
| Sodium Alginate | 30 |
| Sodium Bicarbonate | 50 |
| Calcium Chloride | 30 |
| Ferrous Sulfate | 30 |
| Arizona Test Dust (Grade: A2 Fine) | 420 |
| Dodecylbenzone Sulfonic Acid (Sodium Salt) | 220 |



Feed and Draw Solutions

Surrogate Wastewater Feed Solution

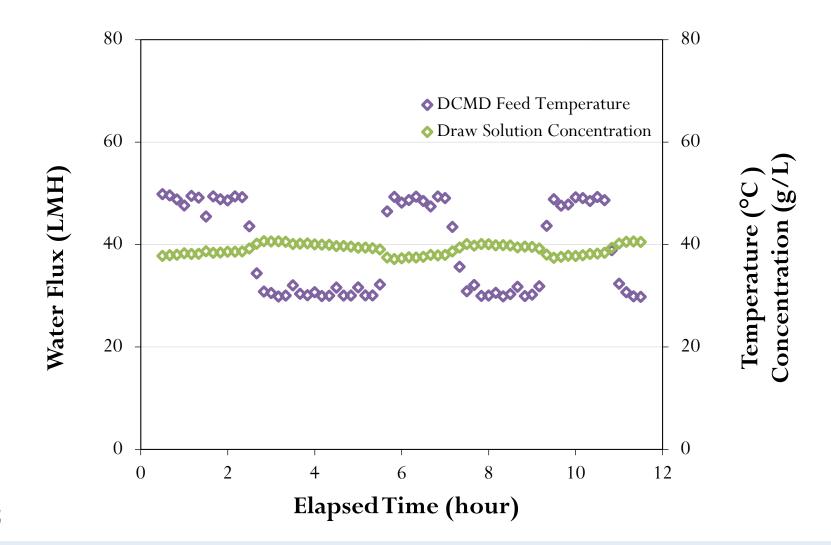
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| Calcium Chloride | 30 |
| Ferrous Sulfate | 30 |
| Arizona Test Dust (Grade: A2 Fine) | 420 |
| Dodecylbenzone Sulfonic Acid (Sodium Salt) | 220 |

Draw Solutions

- Sodium Chloride (NaCl)
- Magnesium Chloride (MgCl₂)
- Sodium Propionate (NaC3H5O2)

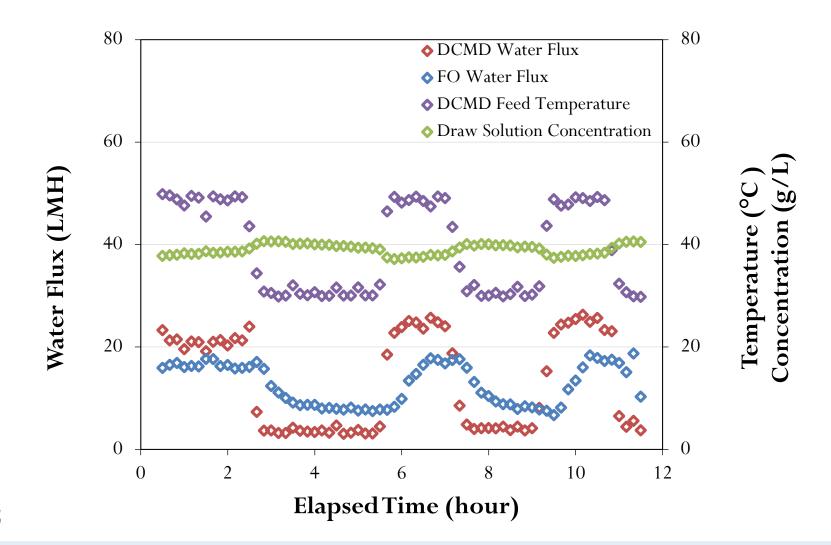


Water Fluxes and System Stability



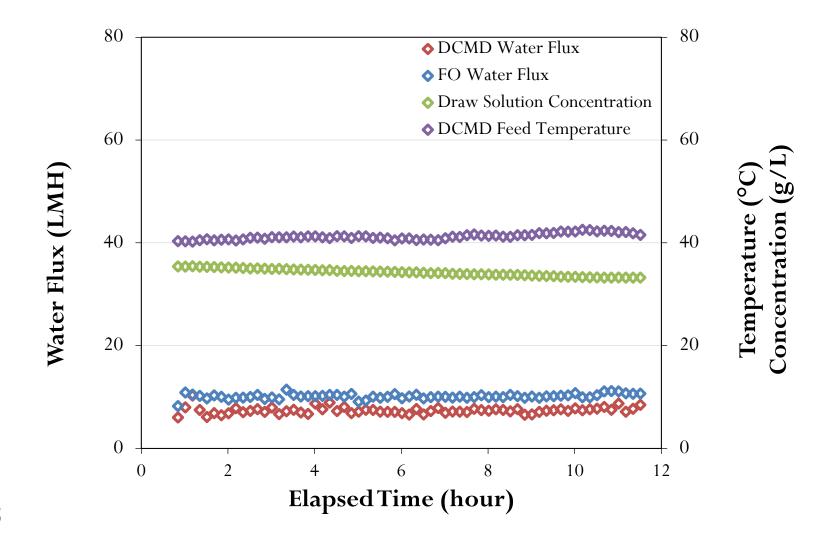


Water Fluxes and System Stability





Water Fluxes and System Stability





Water Quality

Rejection Results of Total Nitrogen (TN) and Total Organic Carbon (TOC)

| | Forward Osmosis (FO) Rejection | | Membrane Distillation (MD) Rejection | | n Rejection |
|-----|--------------------------------|-----|---|-----|-------------|
| TOC | TN | TOC | TN | TOC | TN |
| 97% | 68% | 68% | 97% | 98% | 98% |





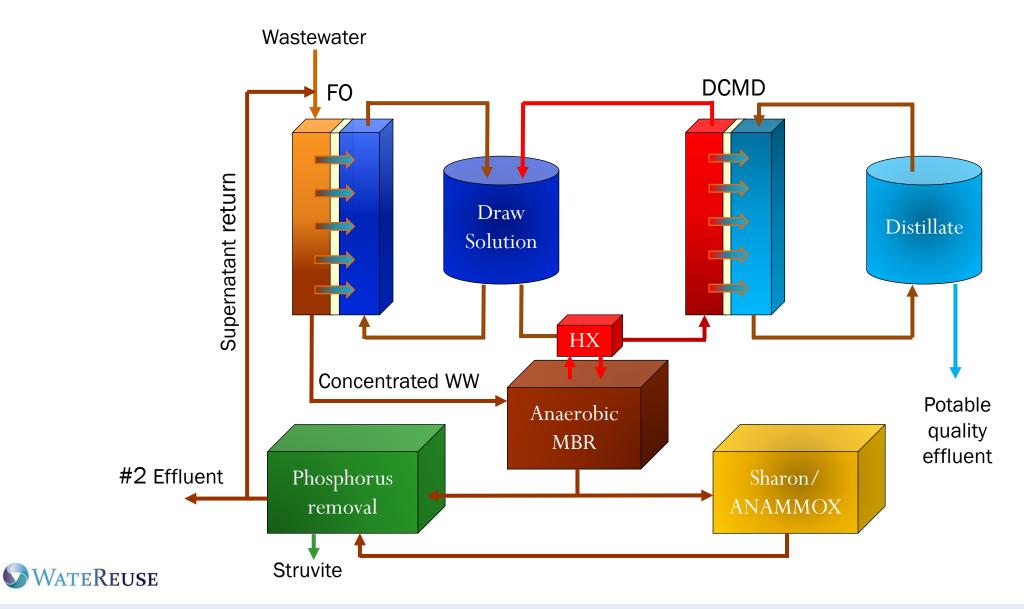


Wastewater Concentration by Forward Osmosis

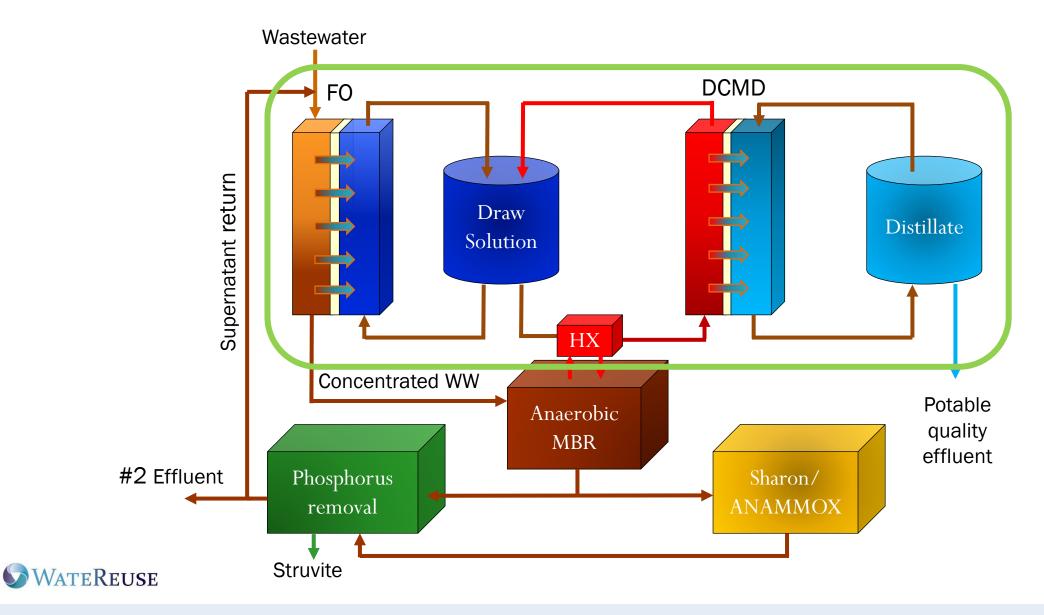
Dr. Sage Hiibel



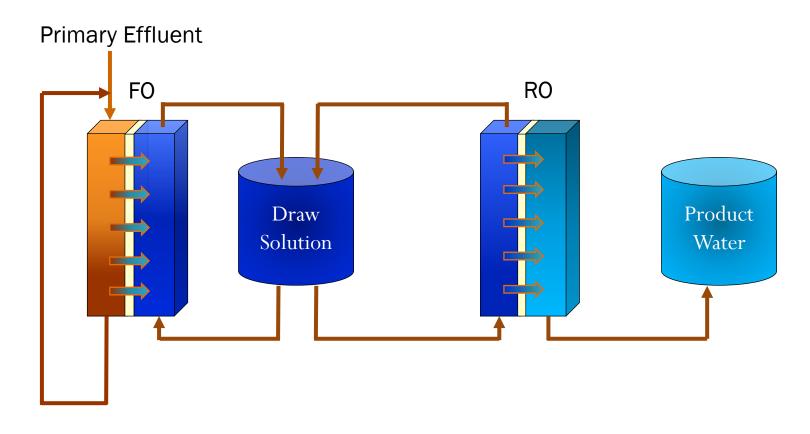
Wastewater Concentration by FO



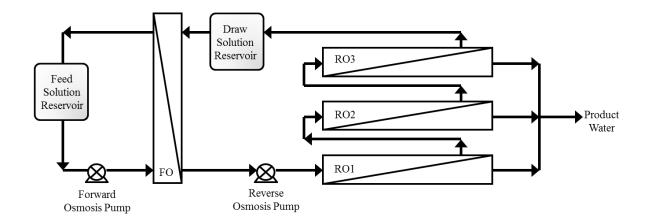
Wastewater Concentration by FO



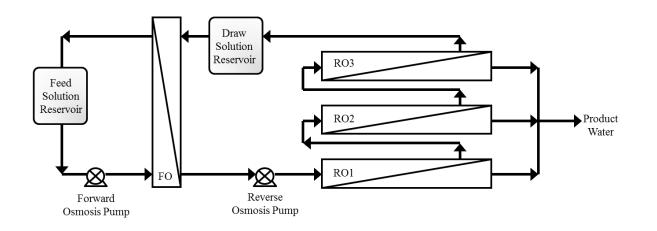
RO for Draw Solution Reconcentration





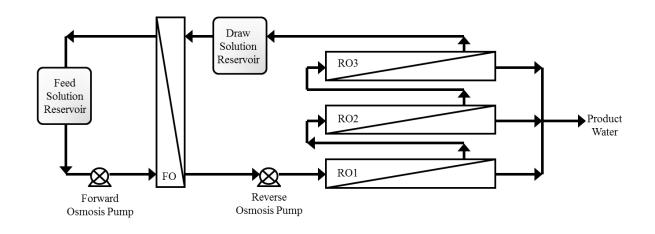






| Experimental Conditions | | |
|--------------------------------|---|---------------------------------|
| Draw Solution | = | 40-45 g/L NaCl |
| Pump Flow Rates | = | 16.5 L/min |
| FO Membrane Area | = | 1.5 m^2 |
| RO Membrane Area (3 in series) | = | $1.5 \text{ m}^2 \text{ total}$ |
| RO Operating Pressure | = | 400 psi |
| Operating Temperature | = | 20-22 °C |



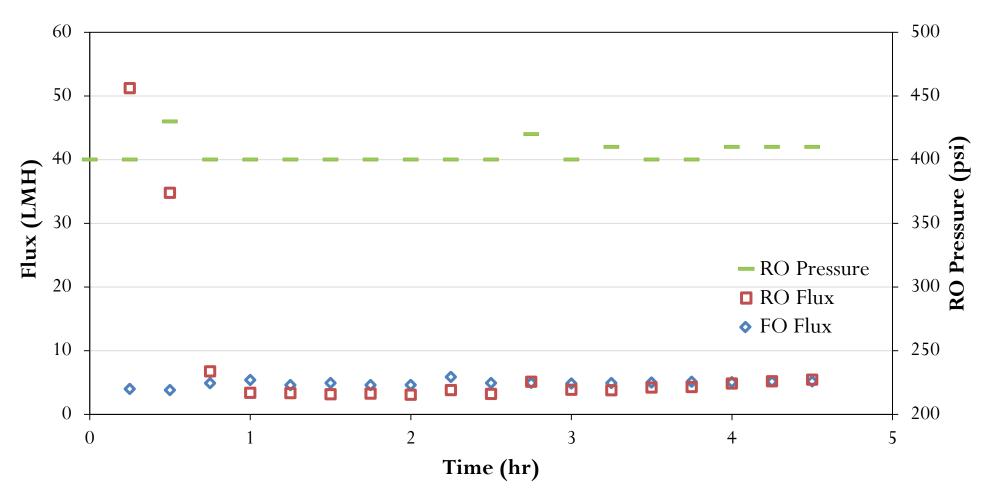


| Experimental Conditions | | | | |
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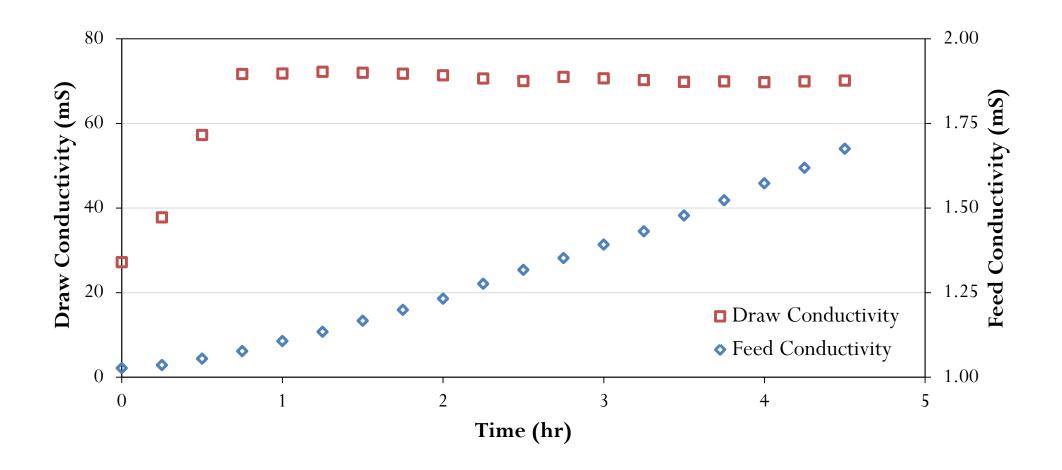


Membrane Flux



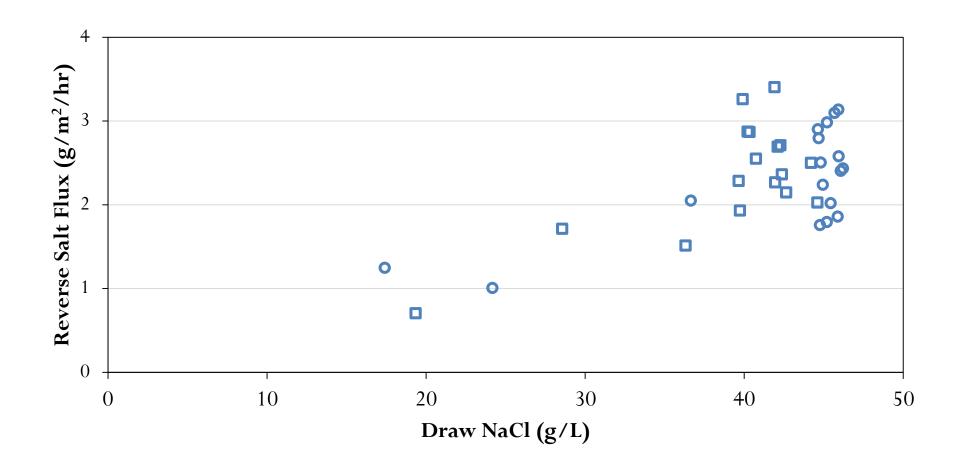


Conductivity





Reverse Salt Flux



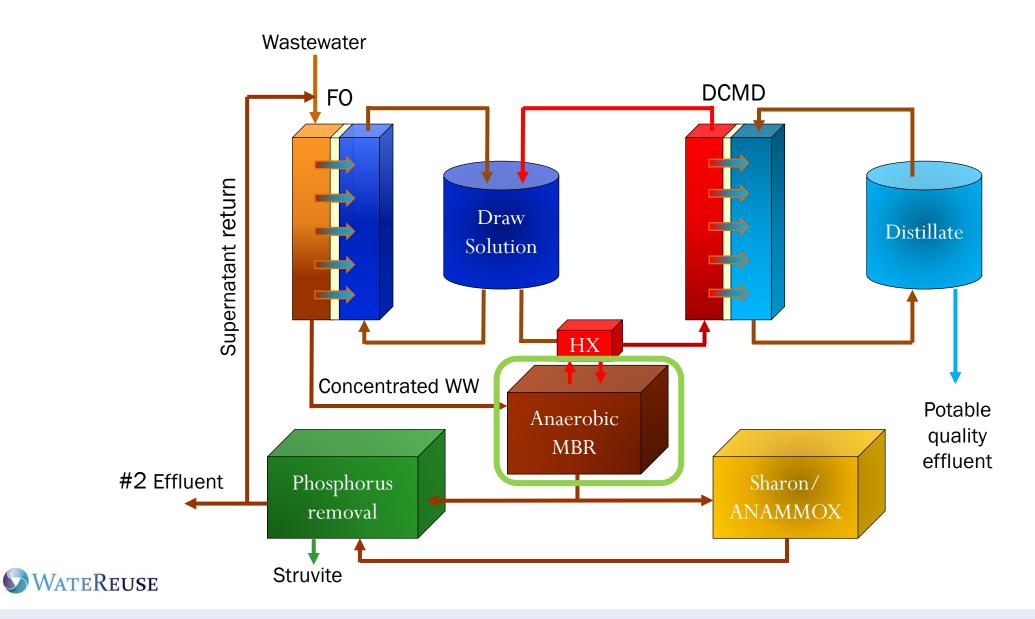


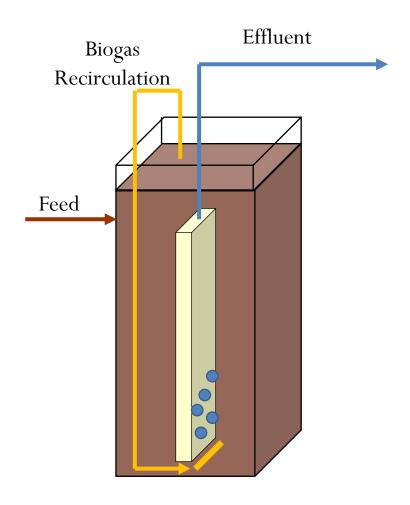
Water Quality

Total Organic Carbon and Total Nitrogen Rejection

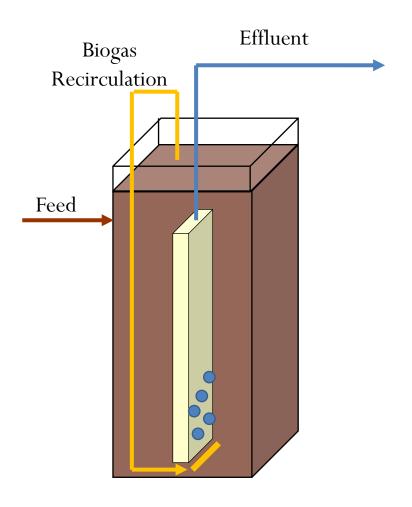
| Pilot-So | cale FO | Pilot-Scale FO-RO System | | |
|----------|---------|-----------------------------|-----|--|
| TOC | TN | TOC | TN | |
| 90% | 84% | 94% | 85% | |





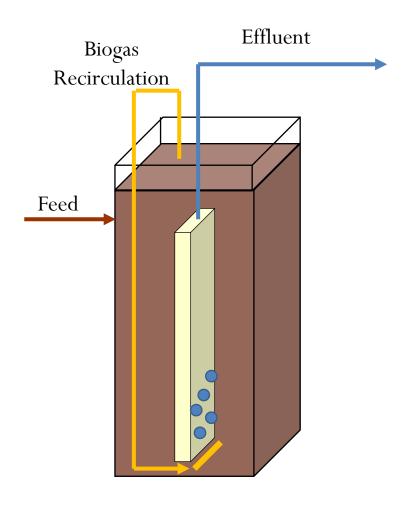






- Biogas recirculation
 - Control membrane fouling
- Four experimental conditions
 - Temperature
 - Wastewater strength



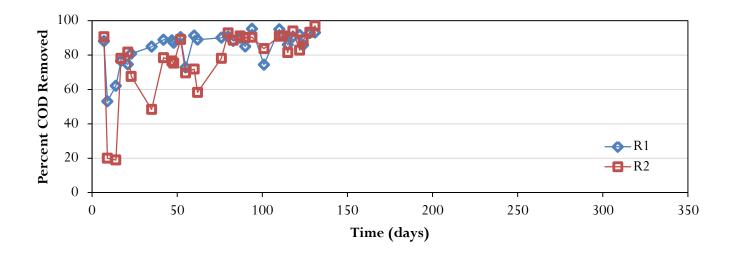


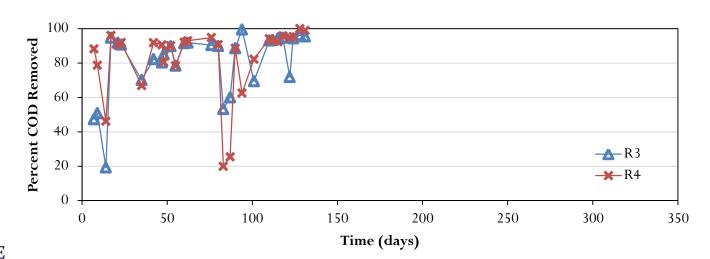
- Biogas recirculation
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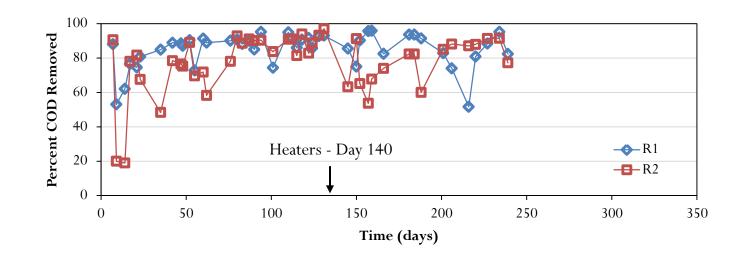
Reactor Performance



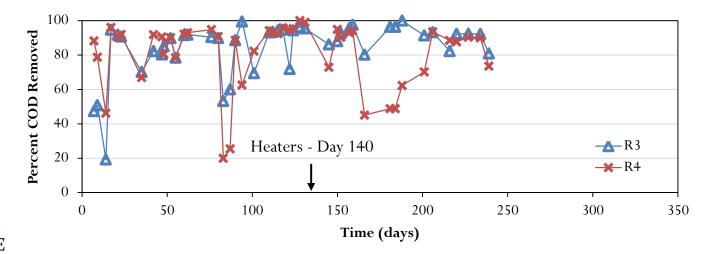




Reactor Performance

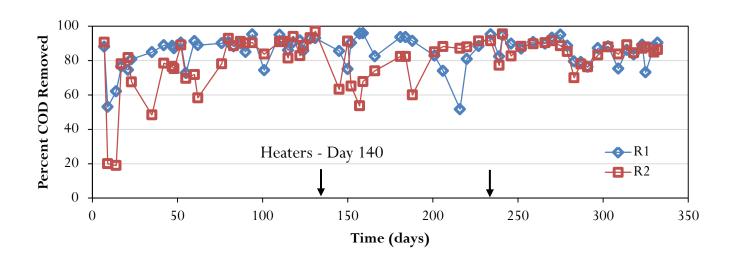




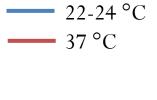


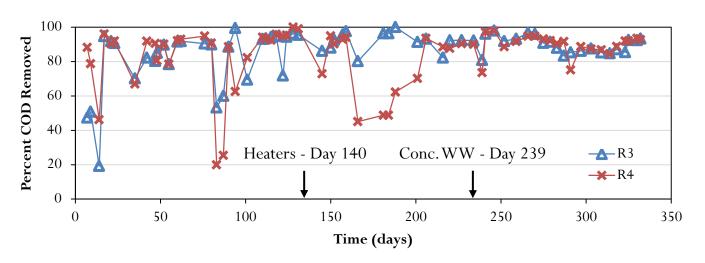


Reactor Performance



Primary Effluent





Concentrated Wastewater



90 Day Average COD Removal

| | Primary | Effluent | Concentrated Wastewater | | |
|-----------------|---------|----------|-------------------------|---------|--|
| Influent COD | 248 1 | mg/L | 357 mg/L | | |
| Condition | Ambient | 37°C | Ambient | 37°C | |
| Effluent COD | 36 mg/L | 37 mg/L | 35 mg/L | 34 mg/L | |
| Percent Removal | 86% | 86% | 90% | 91% | |



Specific Energy Comparisons

| | Forward Osmosis | | Direct Contact Membrane Distillation | | Anaerobic Membrane Bioreactor | |
|-------|-----------------|--------------------|---|----------------------|----------------------------------|-------------------------------------|
| | kWh/m³ | Primary Energy Use | kWh/m³ | Primary Energy Use | kWh/m³ | Primary Energy Use |
| Bench | 3.36 | Pumping | 1,664 | Thermal and Pumping | 111.4 | Pumping and Biogas Recirculation |
| Pilot | 0.23 | Pumping | 2,000 | Thermal ⁺ | 1-5 | Recirculation* |



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Expected offset from pilot-scale AnMBR biogas production = $0.65-1.14 \text{ kWh/m}^3$



Conclusions

- FO/DCMD System
 - High nutrient and organic carbon rejection
 - Temperature has strongest influence over flux
 - Reverse salt flux
- AnMBR
 - High COD removal
 - No detrimental temperature effects observed
- Energy Considerations
 - Biogas production can offset electrical requirements
 - On-site waste heat for DCMD thermal energy requirements







Q & A Period

Submit questions via the chat box

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